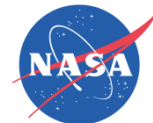




Update on the Progress of Hygrothermal Aging of Triaxial Braided Carbon/Epoxy Composites

Lee W. Kohlman, Duane M. Revilock, Charles R. Ruggeri, J.
Michael Pereira, and Gary D. Roberts
NASA Glenn Research Center, Cleveland, Ohio

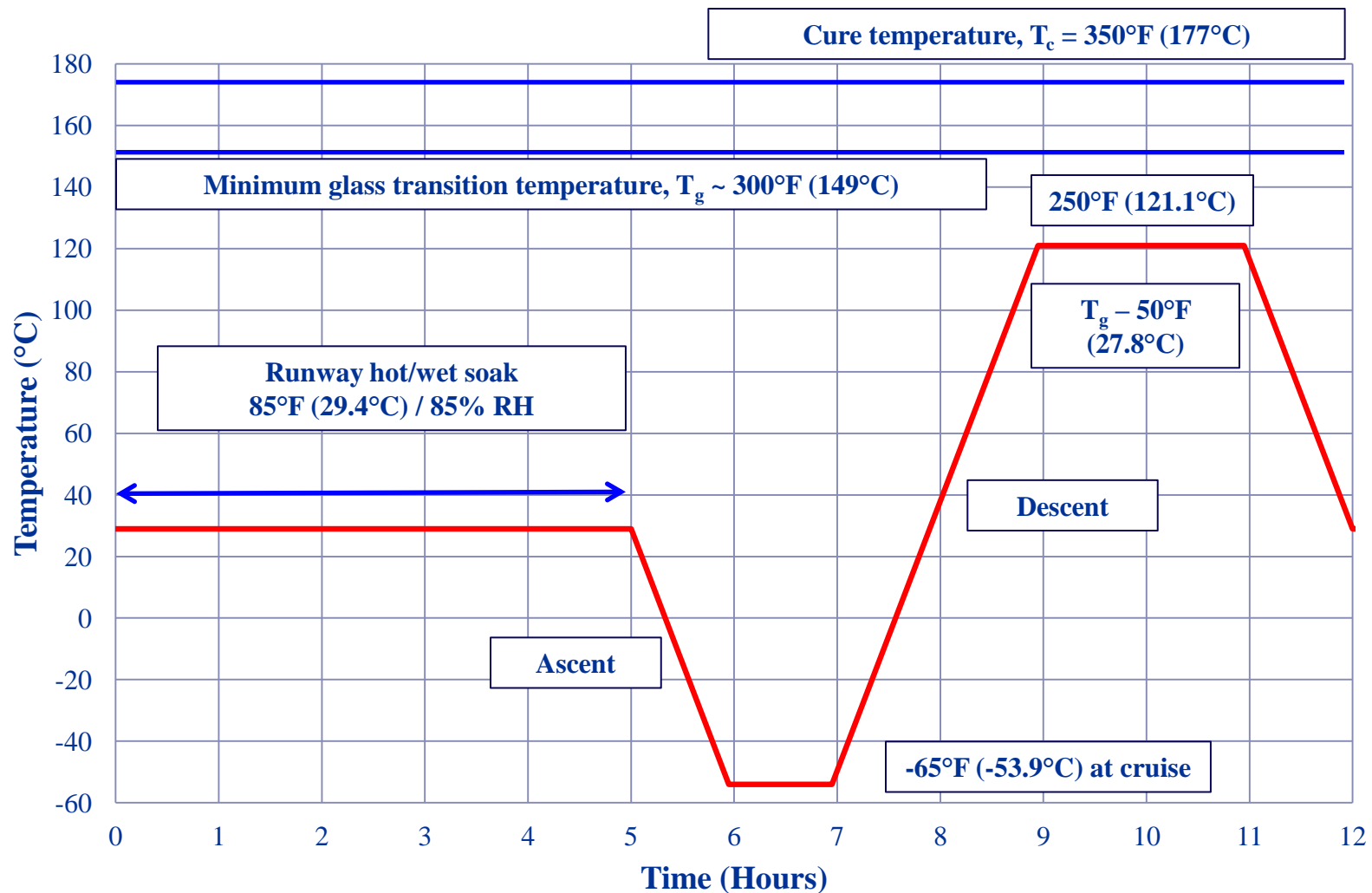


Material Fabrication

- Materials
 - Fiber: Torayca® T700S standard modulus carbon fiber
 - Matrix Materials: 4 ranging from brittle to toughened
 - Hexcel 3502
 - Cytec 5208
 - EPIKOTE Resin 862/EPIKURE Curing Agent W
 - Cytec PR520
- Processing
 - Resin transfer molding (RTM) for both resin and composite
 - Final cure at 350°F (177°C) for 2 hr
 - Resin glass transition temperature, $T_g \geq 300^\circ\text{F}$ (149°C)
 - 6 plies, [+60°/0°/-60°] 2D triaxial braid preform
 - 24k axial tows, 12k bias tows
 - Equal fiber volume in all directions
- Cured composite properties
 - 0.125 in thick, 2'x2' panel
 - ~56% fiber volume fraction



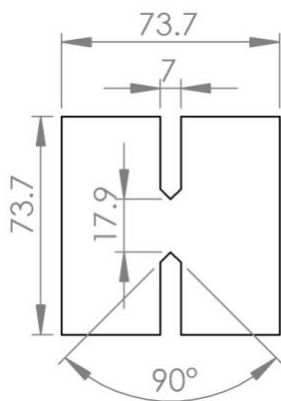
Hygrothermal Aging Cycle



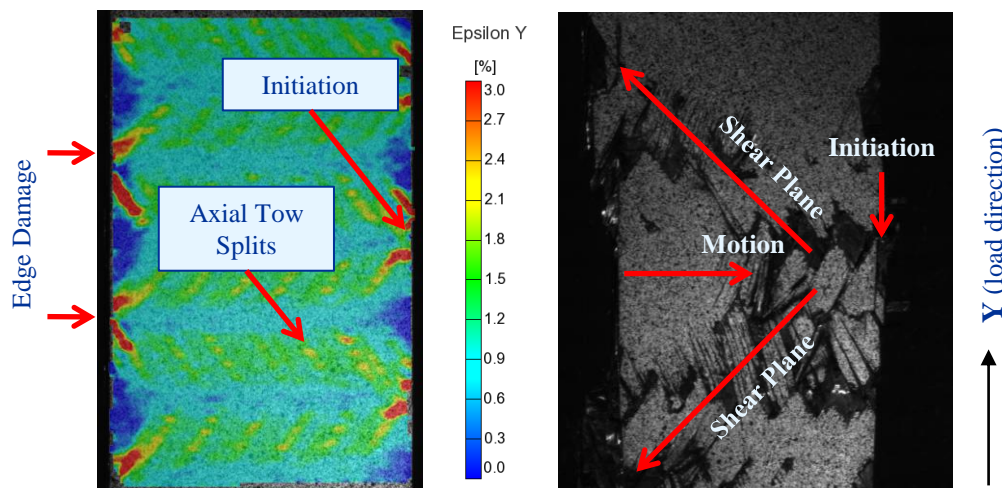
Composite Mechanical Property Test Methods

- ASTM D 3039 Tension
- ASTM D 3410 Compression
- ASTM D 7078 Modified V-Notch Rail Shear

ASTM D 7078
V-Notched
Rail Shear
“H” Specimen



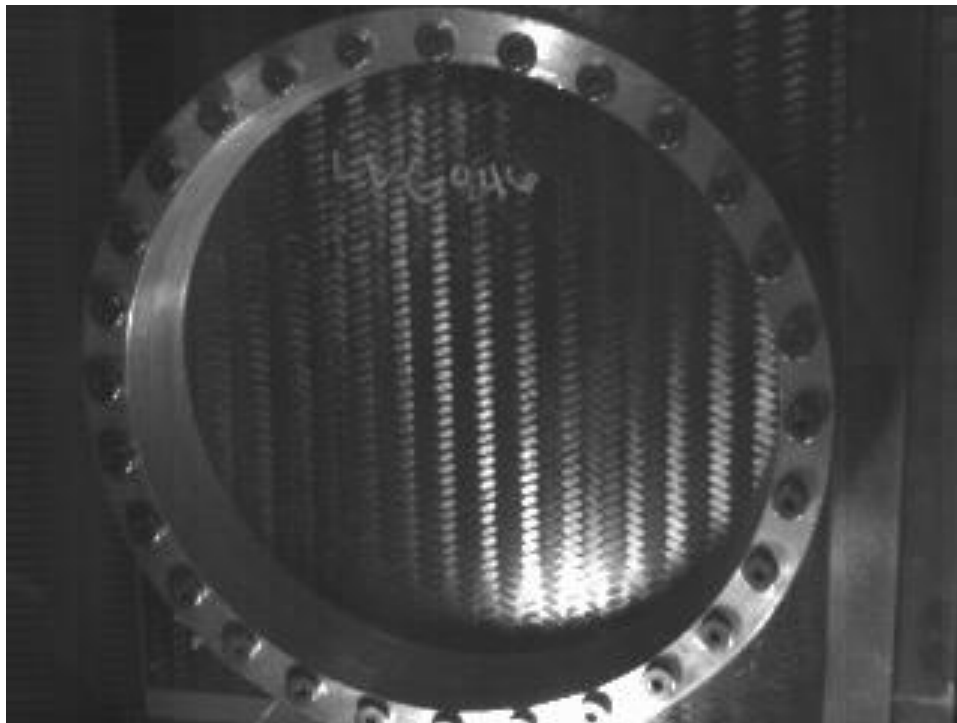
Transverse Tension Test



Test plan limitations

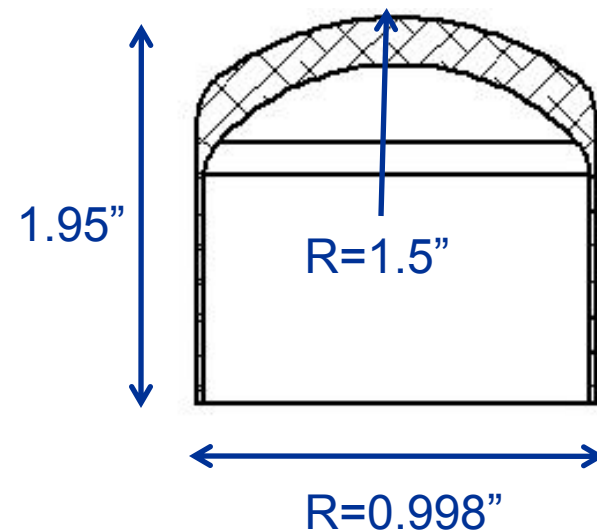
- The number of tests per aging condition was limited by material availability
- The ASTM D 3039 test method does not provide an accurate measure of transverse tensile strength for braided composites
 - Used only to provide an indication of aging effects
 - Improved test methods are being developed

Ballistic Impact Test Method



Test method considerations

- Blunt impact allows large deformation before failure
- Simple method enables easier use in other labs
- 12 in X 12 in panel size provides efficient use of material





Previously Reported E862 Results

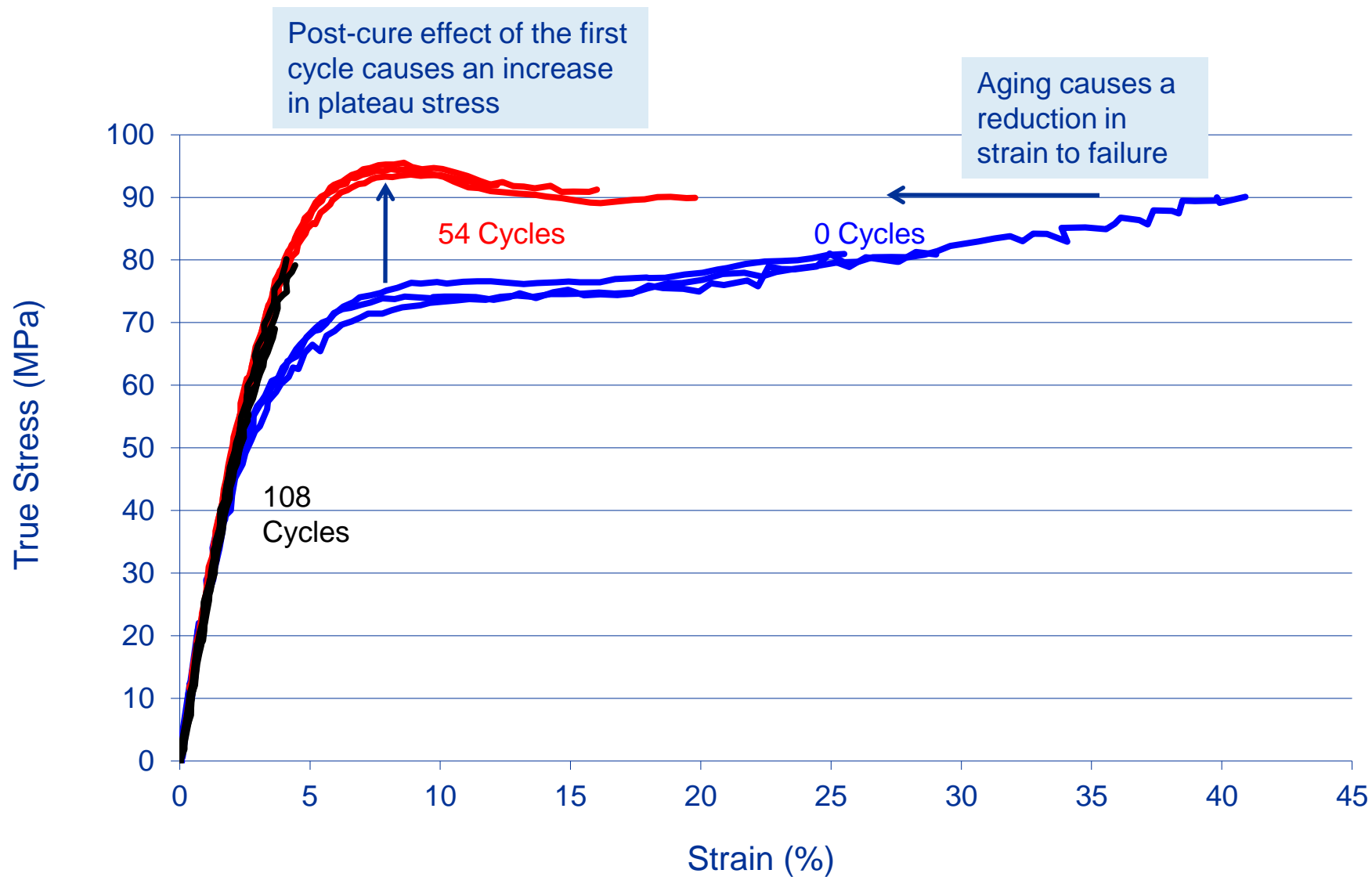


E862 Resin/Composite to 2 Years of Aging

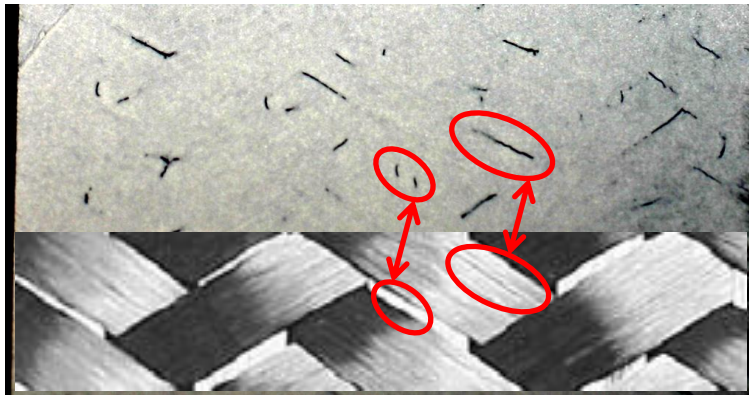
- E862 Resin properties
 - Chemical structure
 - Surface oxidation identified
 - Limited continuation of cure identified
 - Physical properties
 - Glass transition temperature was not affected
 - Physical aging resulting in embrittlement and volume loss identified
 - Mechanical properties
 - Resin tensile strength reduced and ductile response eliminated
- Composite properties
 - Microcracking was observed
 - Mechanical properties
 - Tensile strength was not reduced
 - Compression strength was reduced
 - Shear had not yet been tested
 - Impact penetration threshold was not found to change



E862 Resin Tensile Properties



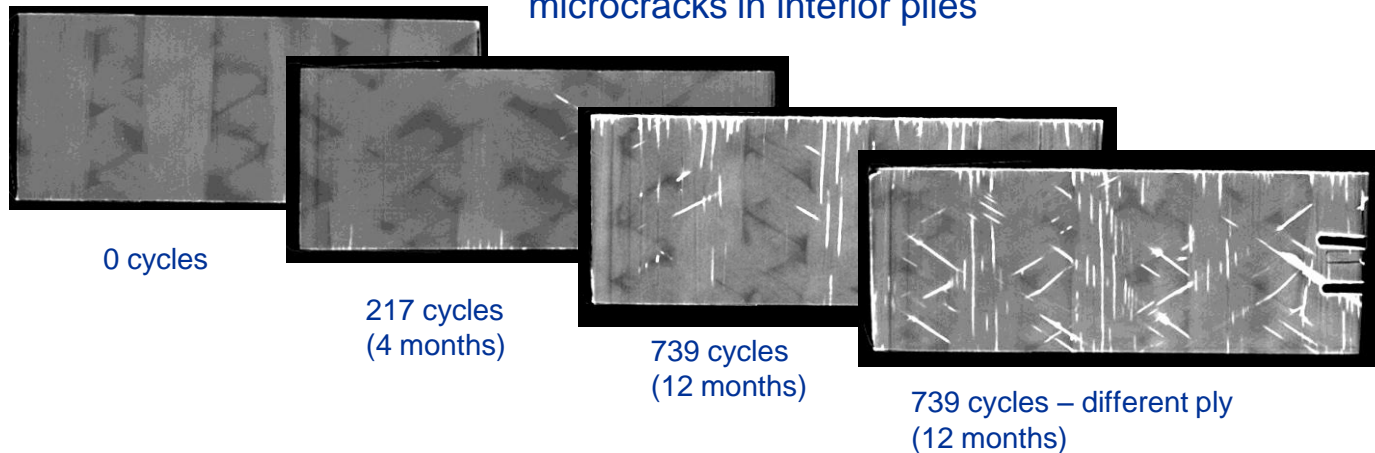
E862 Composite Microcracking



Microcracks
visible on a
painted surface

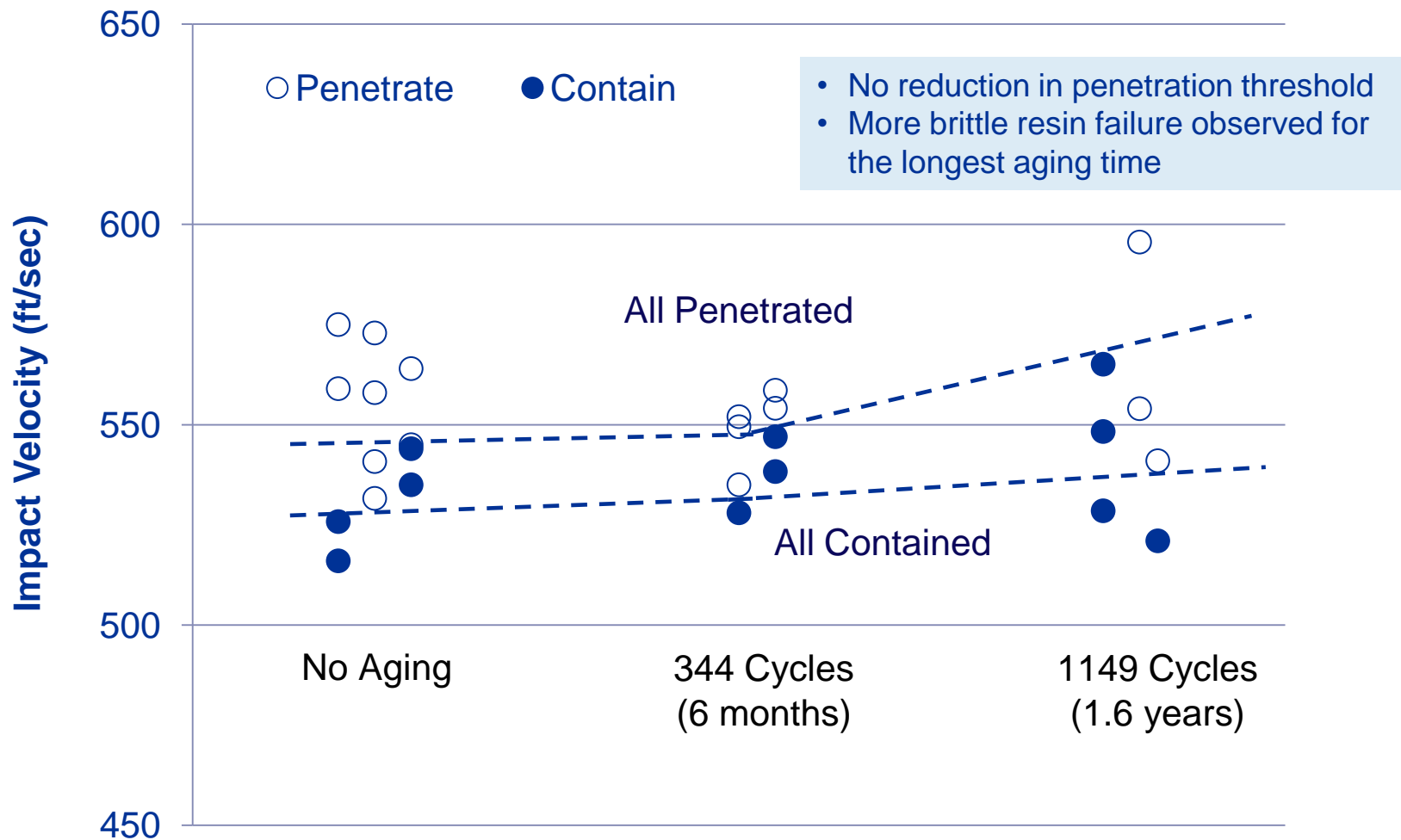
Overlaid image of braid
architecture showing crack
locations within fiber tows

Contrast enhanced X-ray CT images of
microcracks in interior plies





E862 Ballistic Impact Results



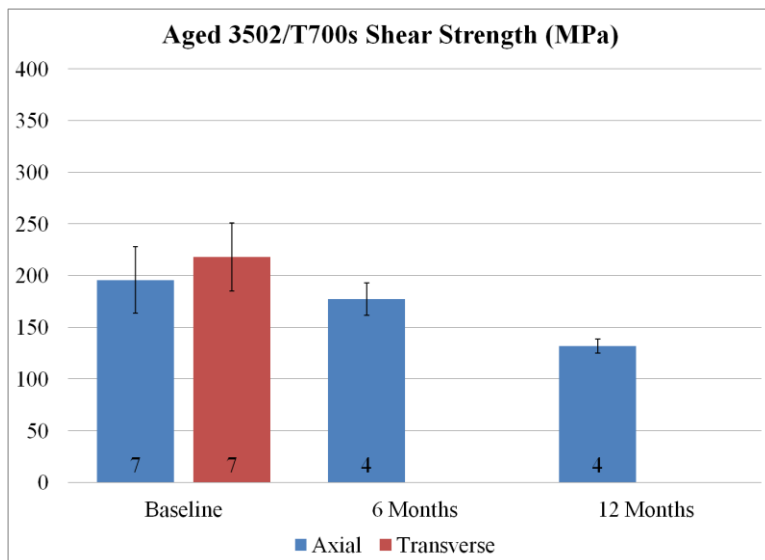
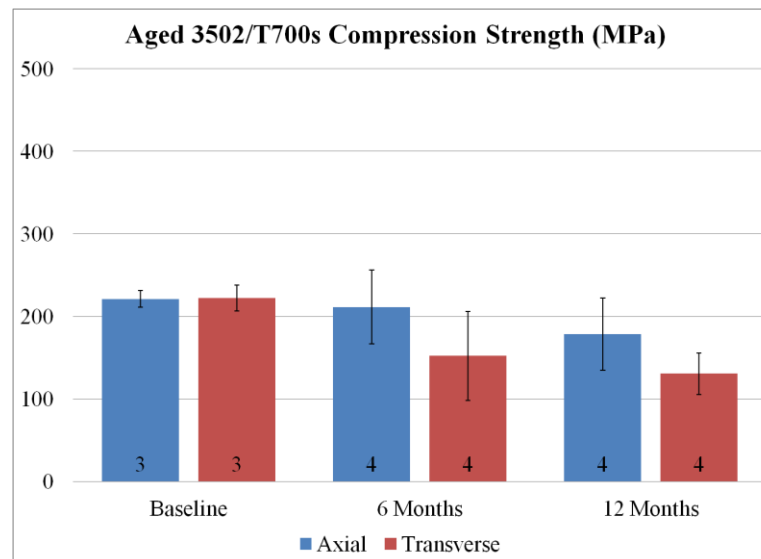
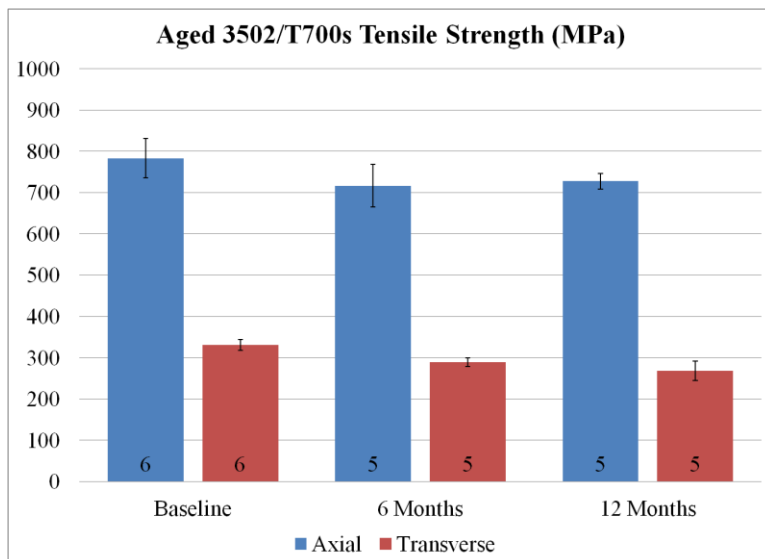


New Mechanical Results

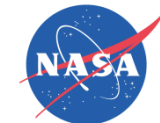
3502, 5208, E862, PR520



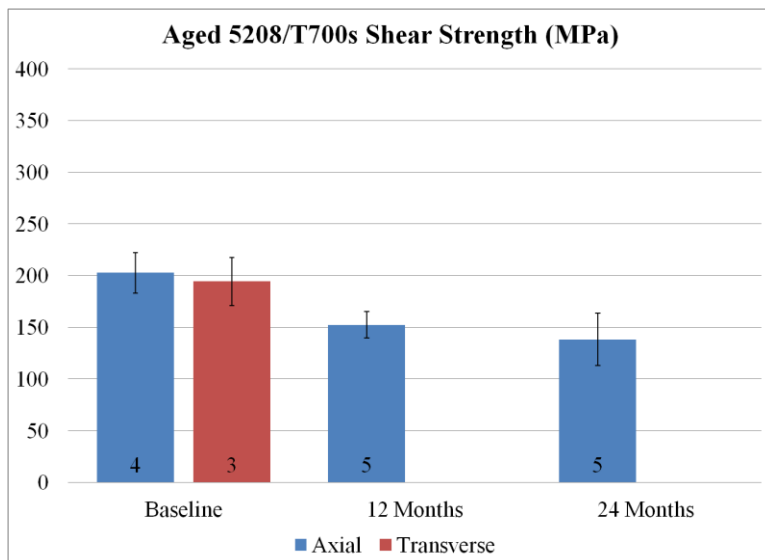
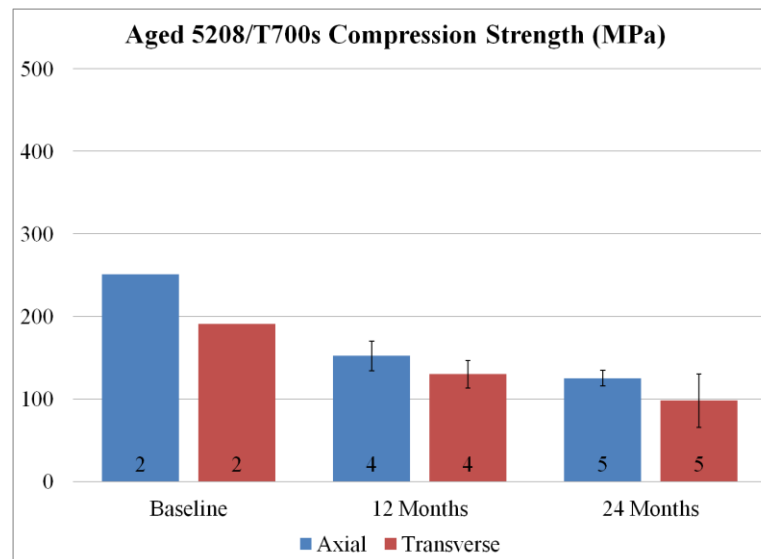
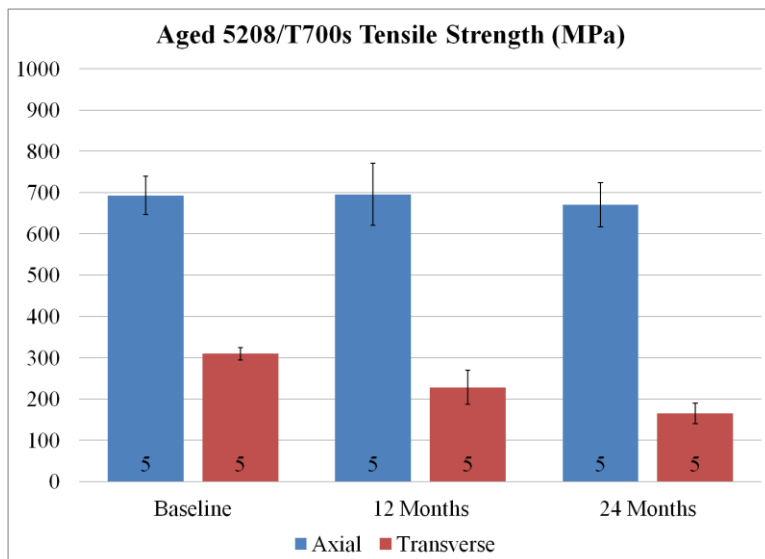
3502 Composite Mechanical Results (12 Months)



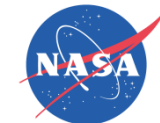
- Possible transverse tension strength reduction
- Shear strength reduction
- Compression strength reduction
- Likely due to observed microcracks initiating failure
- Aging to 24 months is ongoing



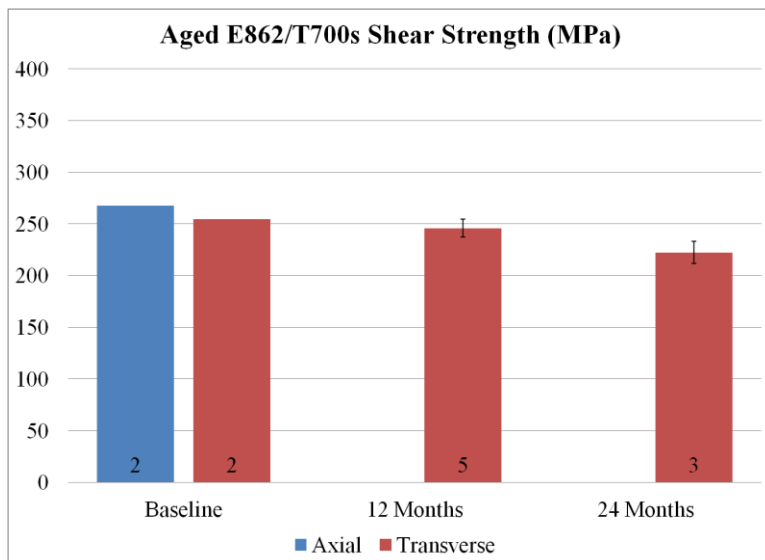
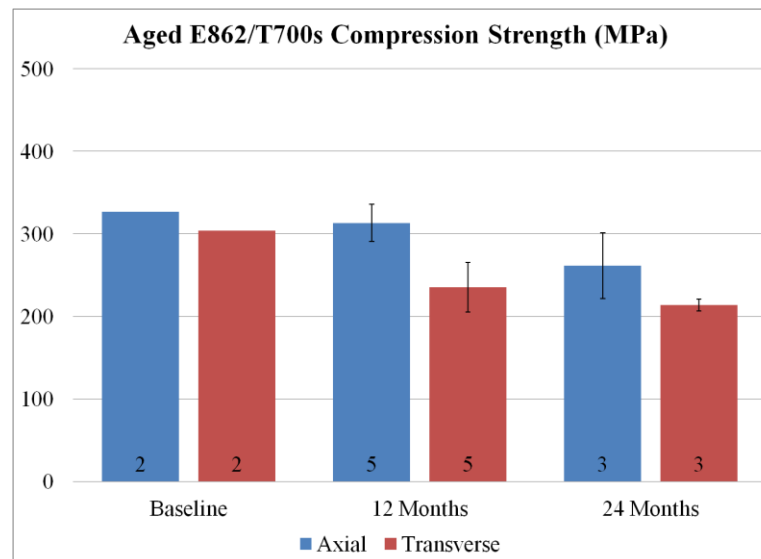
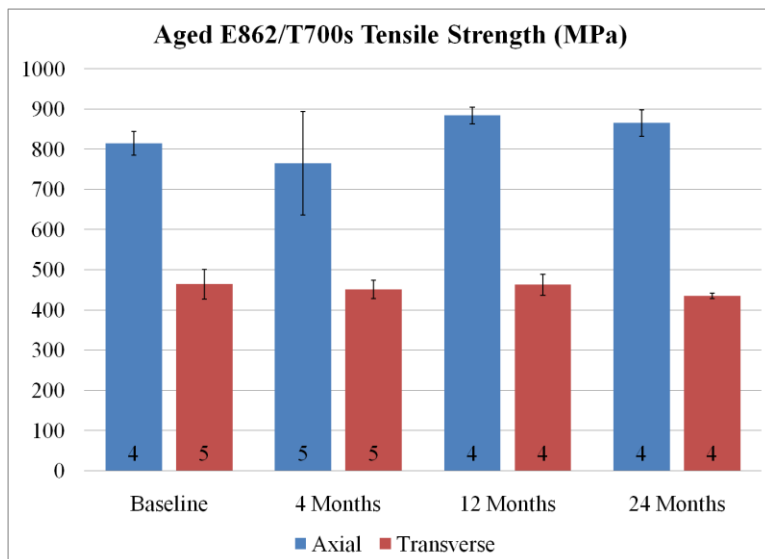
5208 Composite Mechanical Results (24 Months)



- Transverse tensile strength reduction (correlates with shear reduction because of failure mode)
- Shear strength reduction
- Compression strength reduction
- Likely due to observed microcracks initiating failure



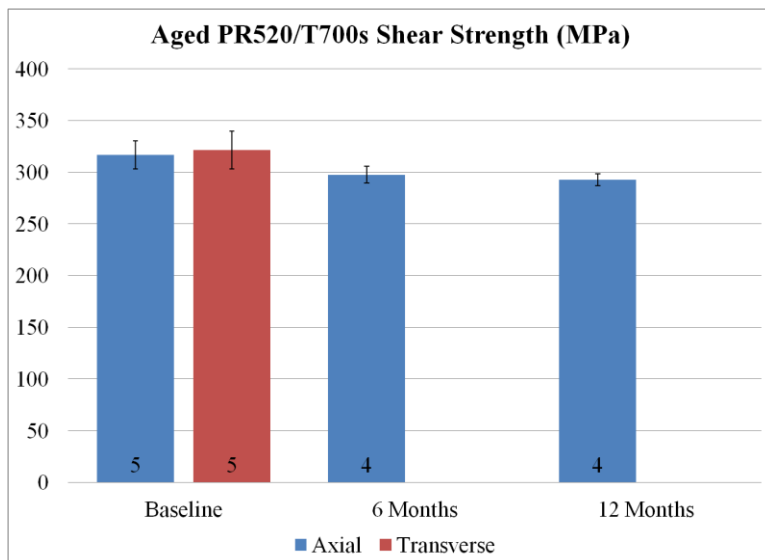
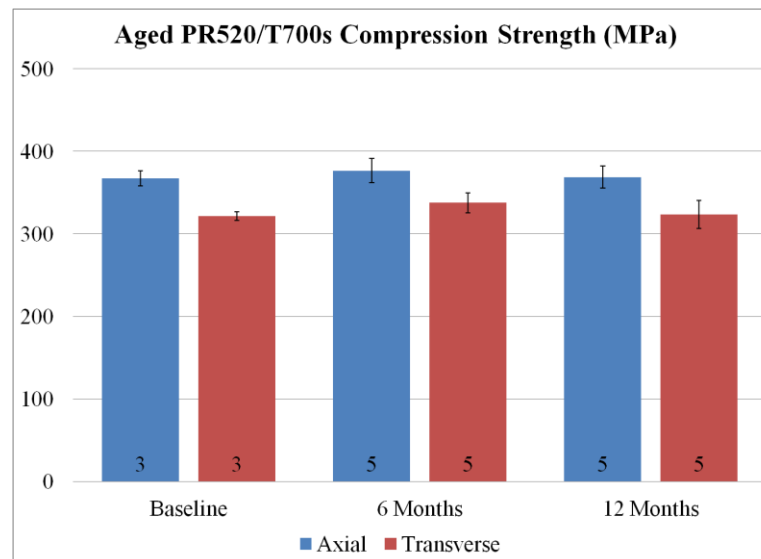
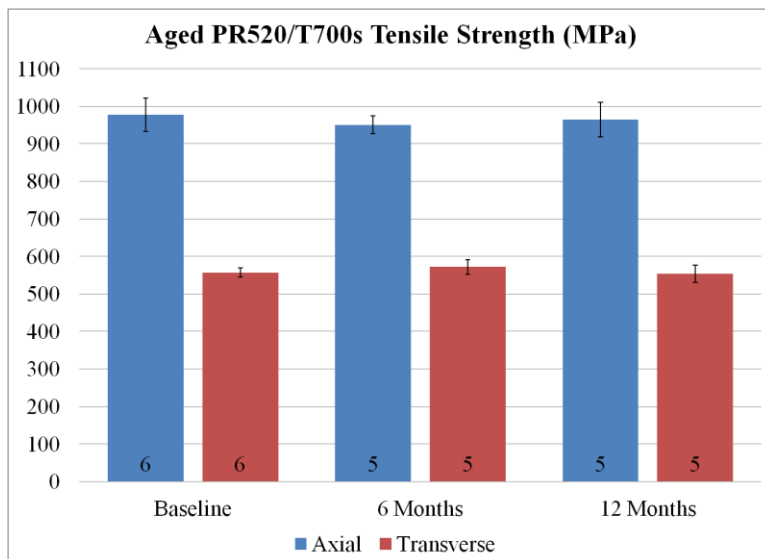
E862 Composite Mechanical Results (24 Months)



- No significant tensile strength changes
- Compression strength reduction likely
- Possible shear strength reduction
- Changes are likely due to observed microcracks initiating failure



PR520 Composite Mechanical Results (12 Months)



- No significant strength changes observed
- Very little evidence of microcracking was observed
- Aging to 24 months is ongoing



Summary of Mechanical Results

- Microcracking has been identified as the most likely cause of strength reduction in compression, shear, and transverse tensile strength
- Previous work with E862 indicated that resin embrittlement can occur
- Preliminary studies indicate that microcracking is occurring during the low temperature part of the cycle as a result of differences in thermal expansion coefficients of fiber and resin

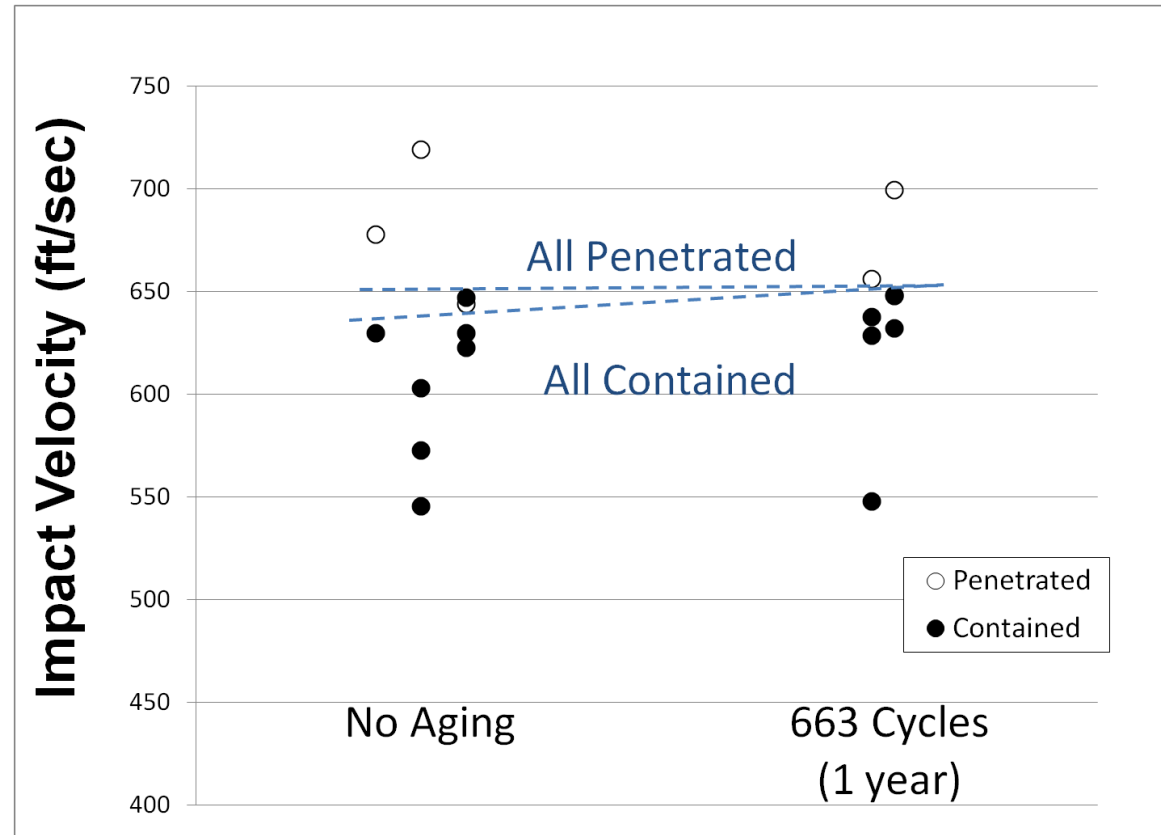


New Ballistic Impact Test Results

3502, PR520

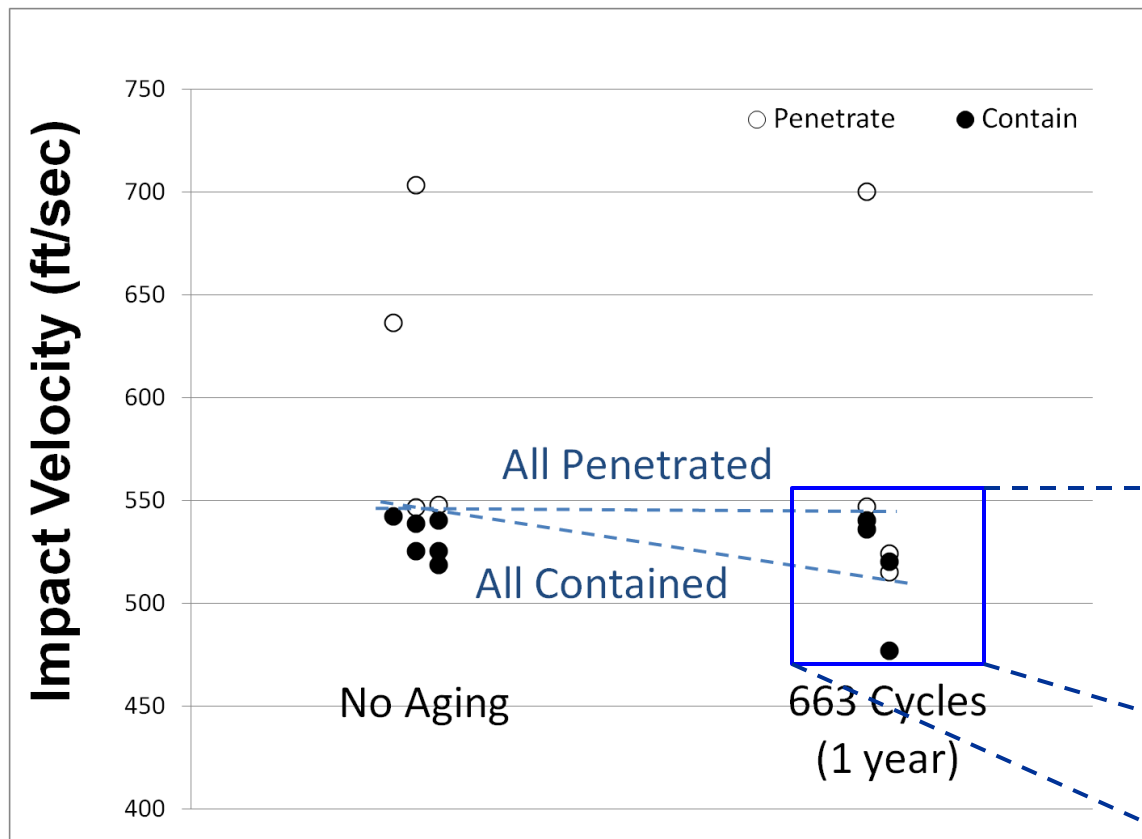
Ballistic Impact Results: 3502

- No aging effect was observed.



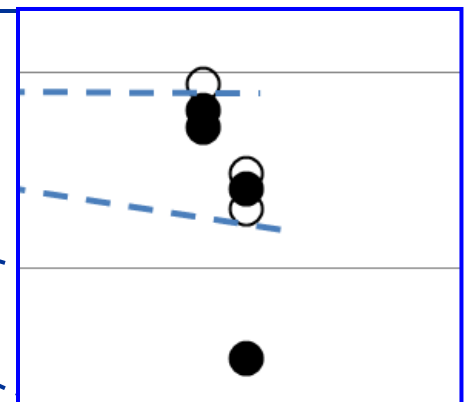
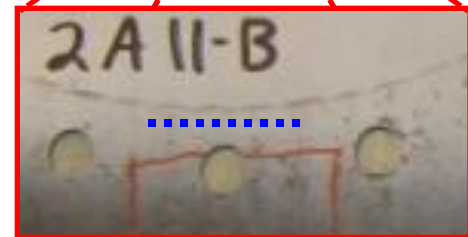
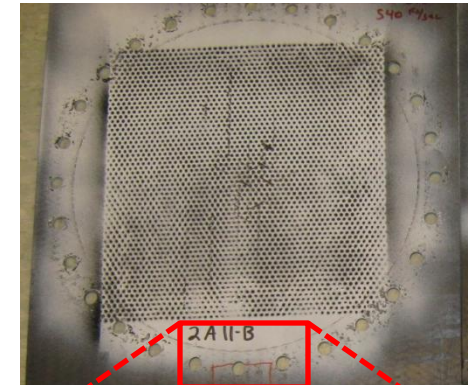
Ballistic Impact Results: PR520

- No aging effect observed.
- Panel variation effect was observed.



Cross Section Location

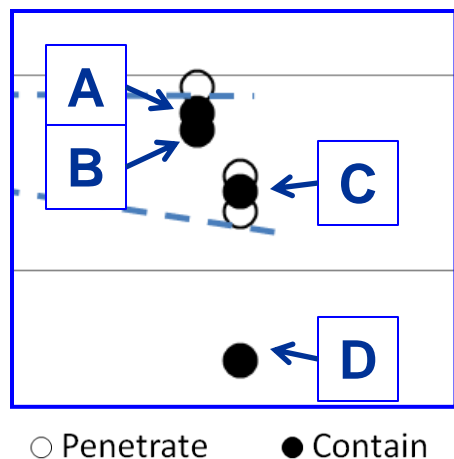
Axial Tows ↑



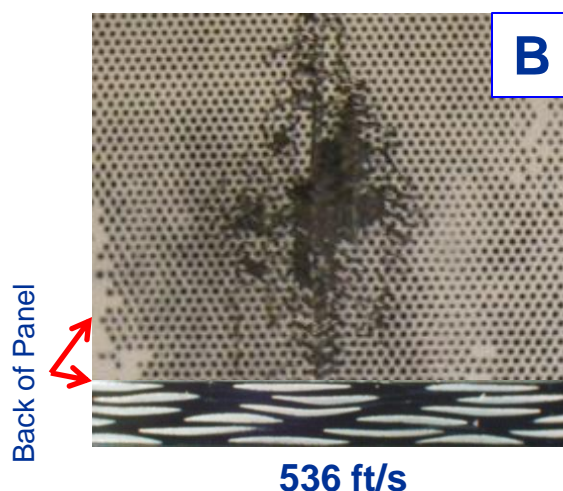
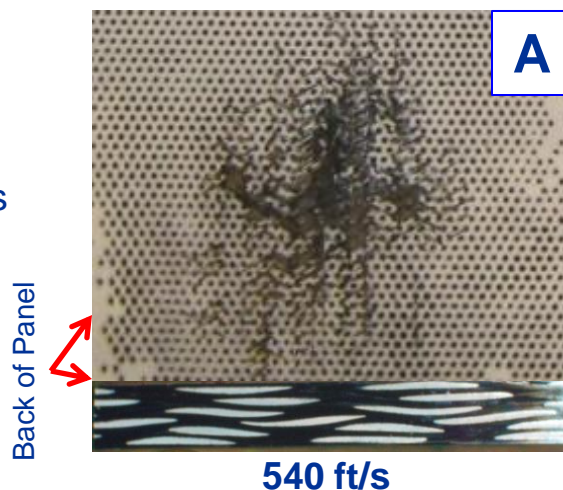
○ Penetrate
● Contain

Impact Damage and Axial Tow Nesting: PR520 Aged

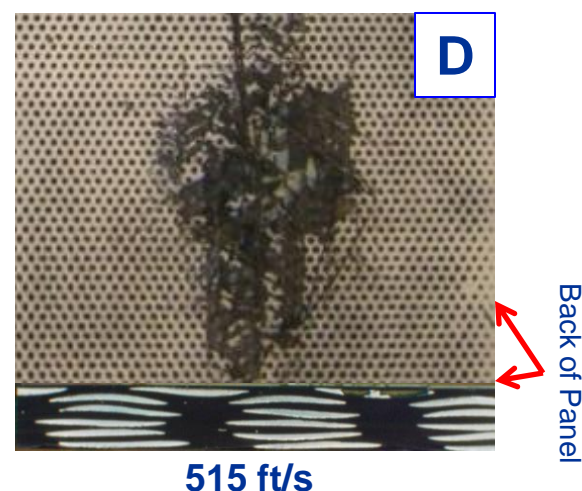
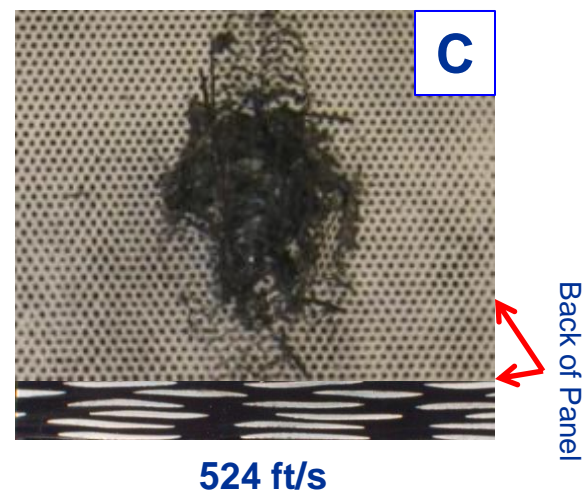
- Nesting is observed by sectioning the panel near the edge, in line with the axial tows passing through the panel center.
- More damage is observed on the side opposite the impact in panels with less axial tow nesting.



Less Damage



More Damage





Summary of Ballistic Impact Results

- Previous aging of the E862 showed little change in impact threshold.
- Additional results on 3502 and PR520 also show little change after 12 months of aging.
- Fiber tow nesting has an influence on impact damage and possibly impact threshold.
- Impact threshold does not correlate with static coupon tests



Conclusions

- Hygrothermal aging has resulted in small reductions in transverse tensile, shear, and compression strengths in E862, 3502, and 5208 composite materials.
- The primary mechanism is the development of microcrack damage that initiates failure in matrix/delamination failure dominated static tests, but not in the fiber failure dominated axial tensile test.
- The impact penetration threshold does not appear to be sensitive to the presence of pre-existing microcrack damage.
- Axial fiber tow nesting can influence the extent of damage following impact and the impact penetration threshold.
- PR520 composite was not observed to be affected by aging up to 12 months; minimal microcrack development was observed.



Continuing Work

- 3502 and PR520 Composite
 - Aging to 2 years
 - Tension
 - Compression
 - Shear
 - Impact
- PR520 Resin
 - Aging to 2 years
 - Tension
 - Compression
 - Shear
 - FTIR, DSC, DMA



The End.